

Topic 5: Transmission Lines

Telecommunication Systems Fundamentals

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Concepts in this Chapter

- *Mathematical Propagation Model for a guided transmission line*
 - *Primary Parameters*
 - *Secondary Parameters*
 - *Bandwidth and Attenuation*
- *Common Transmission Lines*
 - *Copper pair*
 - *Coaxial*
 - *Microstrip*

Theory classes: 1.5 sessions (3 hours)

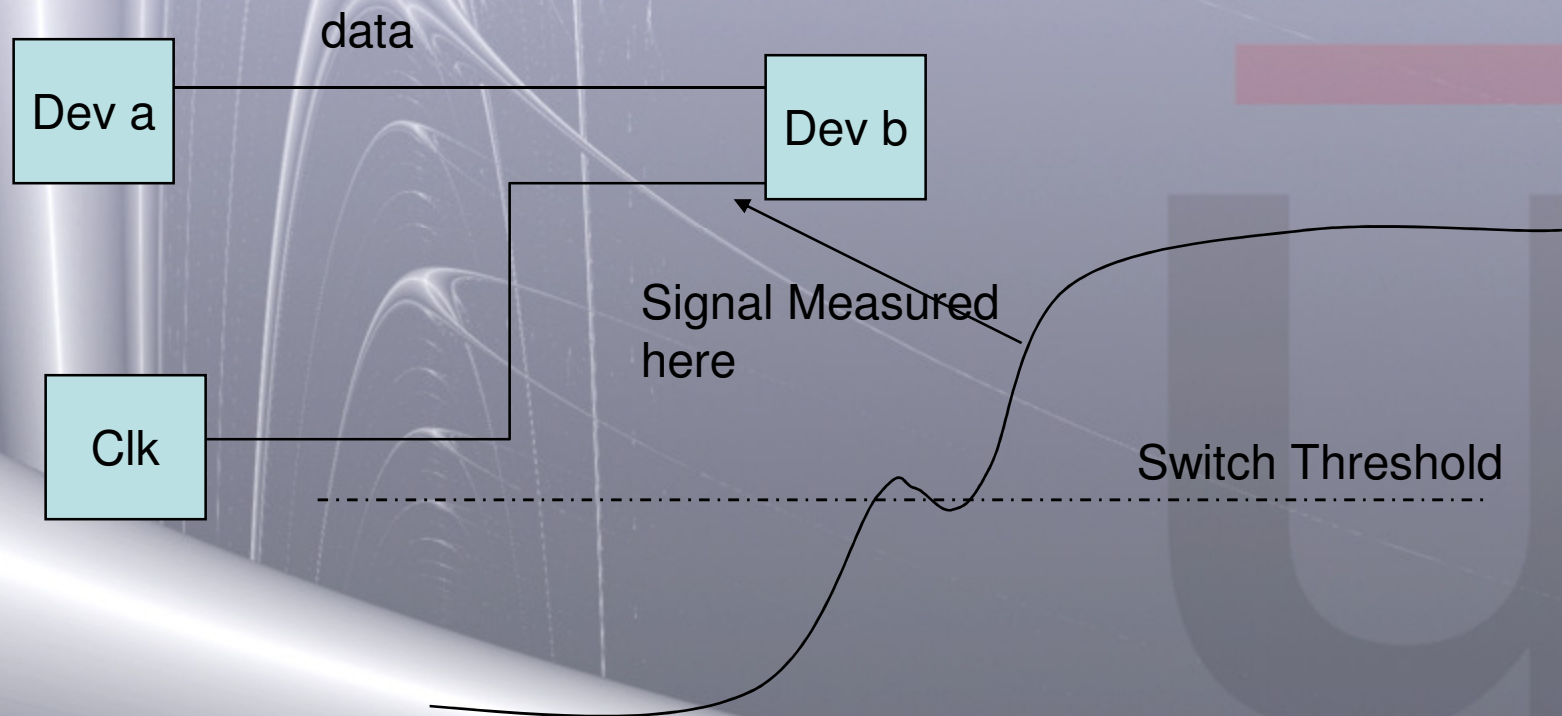
Problems resolution: 0.5 session (1 hour)

Bibliography

- Líneas de Transmisión. Vicente E. Boria. Universidad Politécnica de Valencia.
- Sistemas de Telecomunicación. Transmisión por Línea. J. Hernando Rábanos. Servicio de Publicaciones de la ETSI Telecomunicación UPM

Problem Statement: a practical example

- An engineer tells you the measured clock is non-monotonic and because of this the flip flop internally may double clock the data.

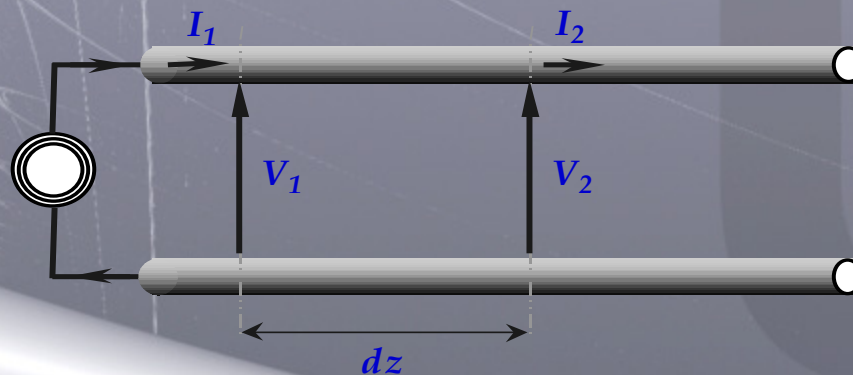


Transmission Line Concept

- Voltage and current on a transmission line is a function of both time and position
 - Must think in terms of position and time to understand transmission line behavior
 - This positional dependence is added when the assumption of the size of the circuit being small compared to the signaling wavelength

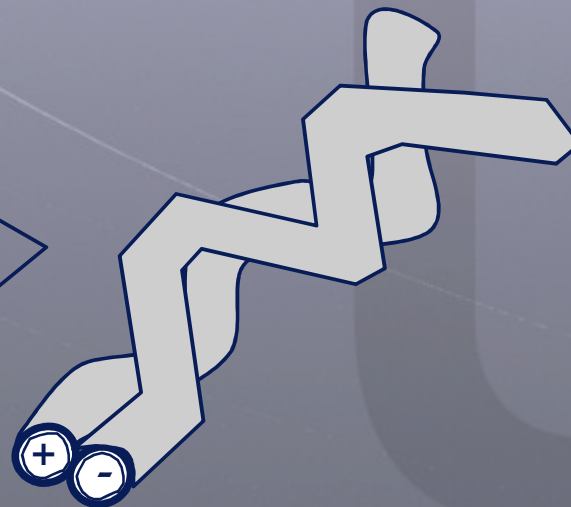
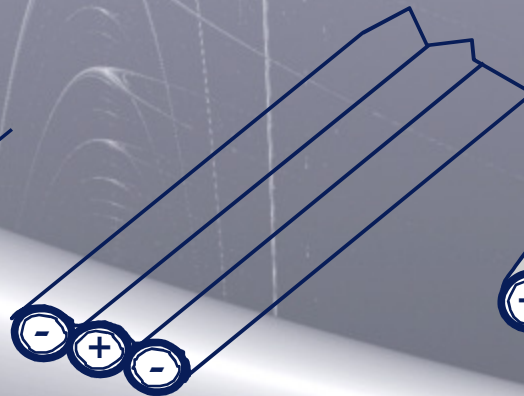
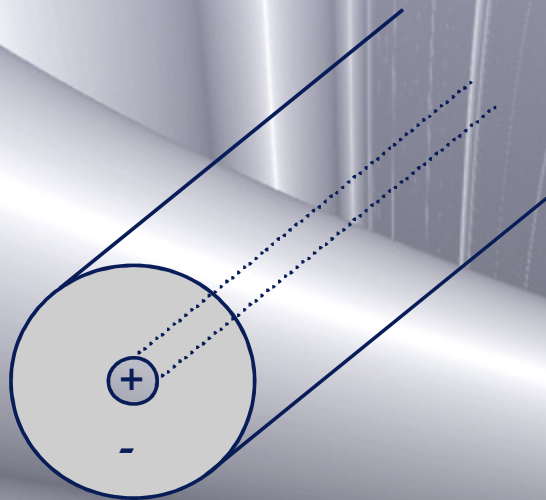
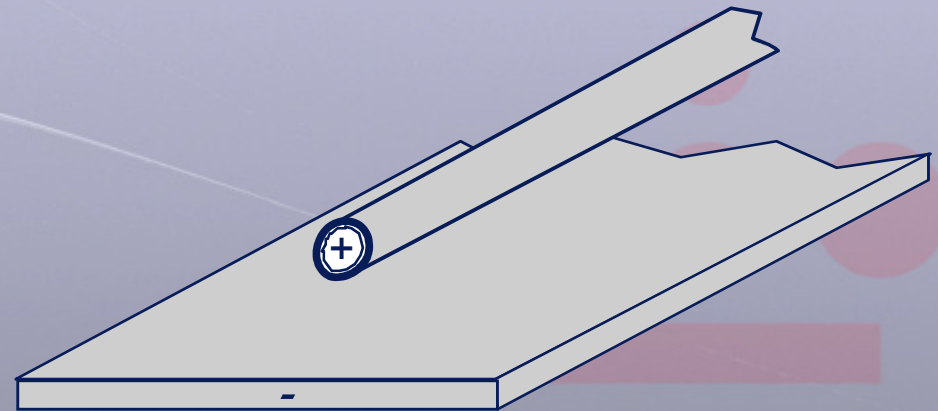
$$V = f(z, t)$$

$$I = f(z, t)$$



Examples of Transmission Lines

- Cables and wires
 - Coax cable
 - Wire over ground
 - Tri-lead wire
 - Twisted pair (two-wire line)
- Long distance interconnects



Transmission Line “Definition”

- General transmission line: a closed system in which power is transmitted from a source to a destination
- In this course we will study only TEM (transversal Electro-Magnetic) mode transmission lines
 - A two conductor wire system with the wires in close proximity, providing relative impedance, velocity and closed current return path to the source
 - Characteristic impedance is the ratio of the voltage and current waves at any one position on the transmission line

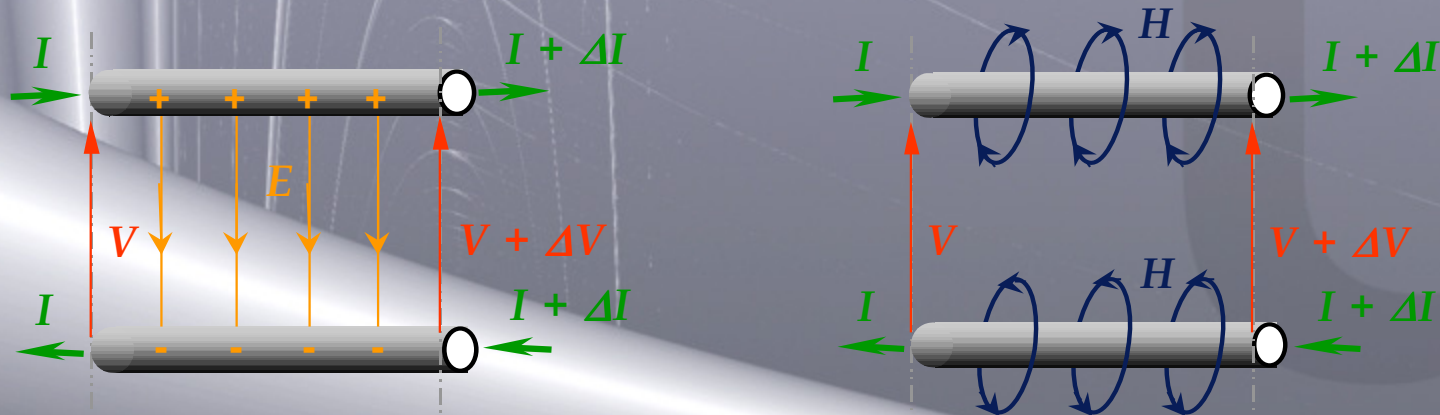
$$Z_0 = \frac{V}{I}$$

- Propagation velocity is the speed with which signals are transmitted through the transmission line in its surrounding medium

$$v = \frac{c}{\sqrt{\epsilon_r}}$$

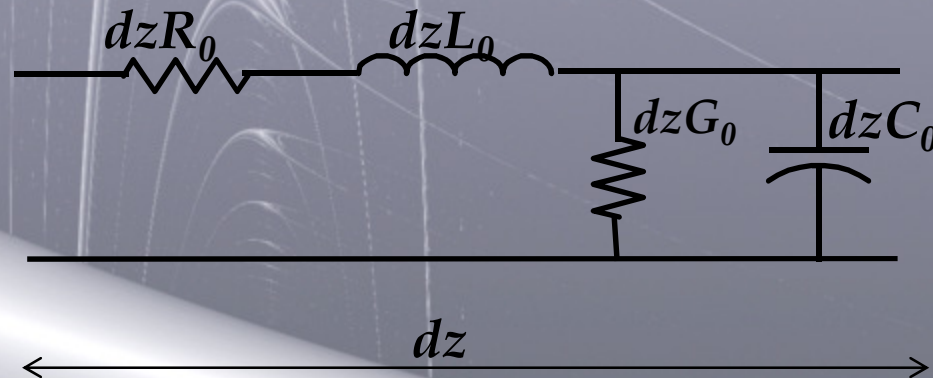
Transmission Lines as a Complex Electromagnetic Problem

- Both Electric and Magnetic fields are present in the transmission lines
 - These fields are perpendicular to each other and to the direction of wave propagation for TEM mode waves, which is the simplest mode
- Electric field is established by a potential difference between two conductors.
 - Implies equivalent circuit model must contain capacitor
- Magnetic field induced by current flowing on the line
 - Implies equivalent circuit model must contain inductor



Transmission Line Equivalent Circuit

- General Characteristics (Primary Parameters)
 - Per-unit-length Capacitance (C_0) [pf/m]
 - Per-unit-length Inductance (L_0) [nf/m]
 - Per-unit-length (Series) Resistance (R_0) [Ω /m]
 - Per-unit-length (Parallel) Conductance (G_0) [$1/\Omega$ m]

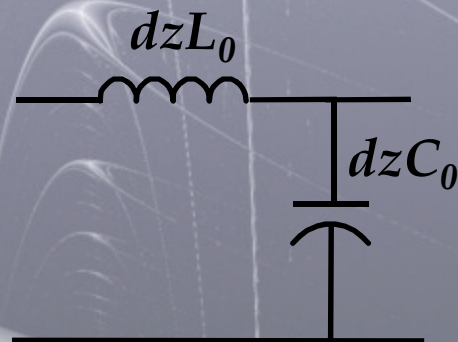


Ideal Transmission Line

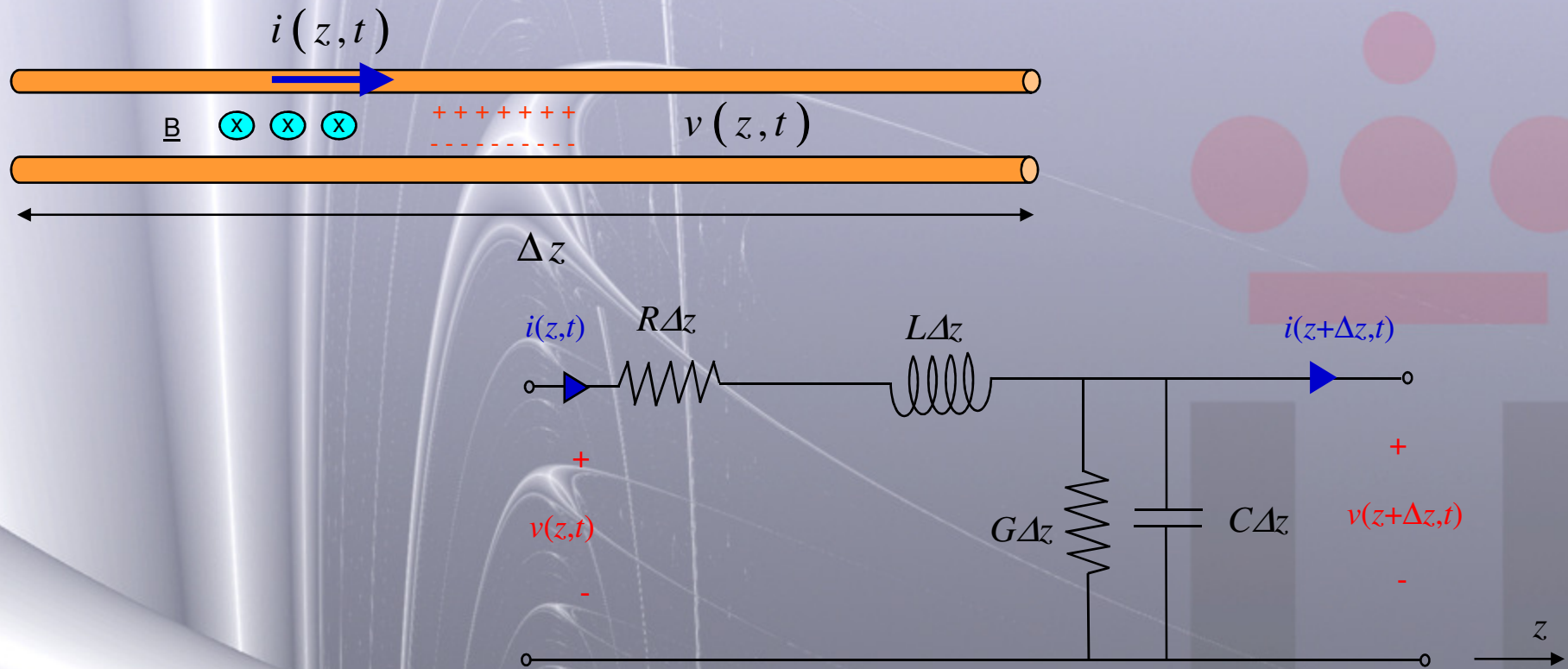
- Ideal (lossless) Characteristics of Transmission Line

- Ideal TL assumes:

- Uniform line
 - Perfect (lossless) conductor ($R_0 \rightarrow 0$)
 - Perfect (lossless) dielectric ($G_0 \rightarrow 0$)



Transmission Line Equivalent Circuit



$$v(z, t) = v(z + \Delta z, t) + i(z, t)R\Delta z + L\Delta z \frac{\partial i(z, t)}{\partial t}$$

$$i(z, t) = i(z + \Delta z, t) + v(z + \Delta z, t)G\Delta z + C\Delta z \frac{\partial v(z + \Delta z, t)}{\partial t}$$

Transmission Line Signal Model

Hence

$$\frac{v(z + \Delta z, t) - v(z, t)}{\Delta z} = -Ri(z, t) - L \frac{\partial i(z, t)}{\partial t}$$

$$\frac{i(z + \Delta z, t) - i(z, t)}{\Delta z} = -Gv(z + \Delta z, t) - C \frac{\partial v(z + \Delta z, t)}{\partial t}$$

Now let $\Delta z \rightarrow 0$

$$\frac{\partial v}{\partial z} = -Ri - L \frac{\partial i}{\partial t}$$

$$\frac{\partial i}{\partial z} = -Gv - C \frac{\partial v}{\partial t}$$

which are known as “Telegrapher’s Equations”

Transmission Line Signal Model

- To combine these, take the derivative of the first one with respect to z :

$$\begin{aligned}\frac{\partial^2 v}{\partial z^2} &= -R \frac{\partial i}{\partial z} - L \frac{\partial}{\partial z} \left(\frac{\partial i}{\partial t} \right) \\ &= -R \frac{\partial i}{\partial z} - L \frac{\partial}{\partial t} \left(\frac{\partial i}{\partial z} \right) \\ &= -R \left[-Gv - C \frac{\partial v}{\partial t} \right] \\ &\quad - L \left[-G \frac{\partial v}{\partial t} - C \frac{\partial^2 v}{\partial t^2} \right]\end{aligned}$$

} Switch the order of the derivatives

Transmission Line Signal Model

$$\frac{\partial^2 v}{\partial z^2} = -R \left[-Gv - C \frac{\partial v}{\partial t} \right] - L \left[-G \frac{\partial v}{\partial t} - C \frac{\partial^2 v}{\partial t^2} \right]$$

- Hence, we have

$$\frac{\partial^2 v}{\partial z^2} - (RG)v - (RC + LG) \frac{\partial v}{\partial t} - LC \left(\frac{\partial^2 v}{\partial t^2} \right) = 0$$

- The same equation also holds for i



$$\frac{d^2 V}{dz^2} - (RG)V - (RC + LG)j\omega V - LC(-\omega^2)V = 0$$

Transmission Line Signal Model

$$\frac{d^2V}{dz^2} = (RG)V + j\omega(RC + LG)V - (\omega^2 LC)V$$

$$RG + j\omega(RC + LG) - \omega^2 LC = (R + j\omega L)(G + j\omega C)$$

$$Z = R + j\omega L \quad = \text{series impedance/length}$$

$$Y = G + j\omega C \quad = \text{parallel admittance/length}$$

- We can re-write

$$\frac{d^2V}{dz^2} = (ZY)V$$

Transmission Line Signal Model

- Defining $\gamma^2 = ZY$
- The differential equation governing the signal is

$$\frac{d^2V}{dz^2} = (\gamma^2)V$$

- Which solution is

$$V(z) = Ae^{-\gamma z} + Be^{+\gamma z}$$

- Where

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$\sqrt{z} = \sqrt{|z|} e^{j\theta/2}$$

$$-\pi < \theta < \pi$$

$$\gamma = \alpha + j\beta$$

$$\alpha \geq 0, \beta \geq 0$$

α = attenuation constant

β = phase constant

Transmission Line Signal Model

- Forward travelling wave (a wave traveling in the positive z direction):

$$V^+(z) = V_0^+ e^{-\gamma z} = V_0^+ e^{-\alpha z} e^{-j\beta z}$$

$$v^+(z, t) = \text{Re} \left\{ \left(V_0^+ e^{-\alpha z} e^{-j\beta z} \right) e^{j\omega t} \right\}$$

$$= \text{Re} \left\{ \left(|V_0^+| e^{j\phi} e^{-\alpha z} e^{-j\beta z} \right) e^{j\omega t} \right\}$$

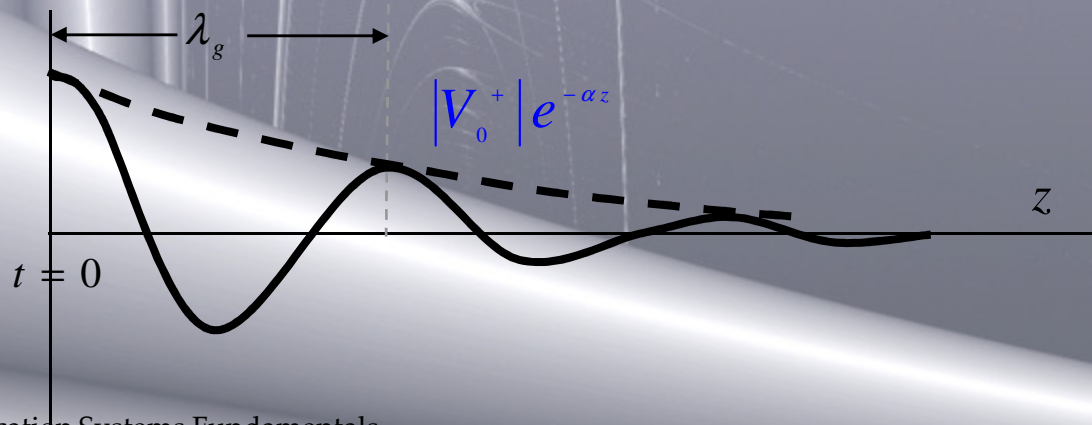
$$= |V_0^+| e^{-\alpha z} \cos(\omega t - \beta z + \phi)$$

The wave “repeats” when

$$\beta \lambda_g = 2\pi$$

Hence:

$$\beta = \frac{2\pi}{\lambda_g}$$



Transmission Line Secondary Parameters

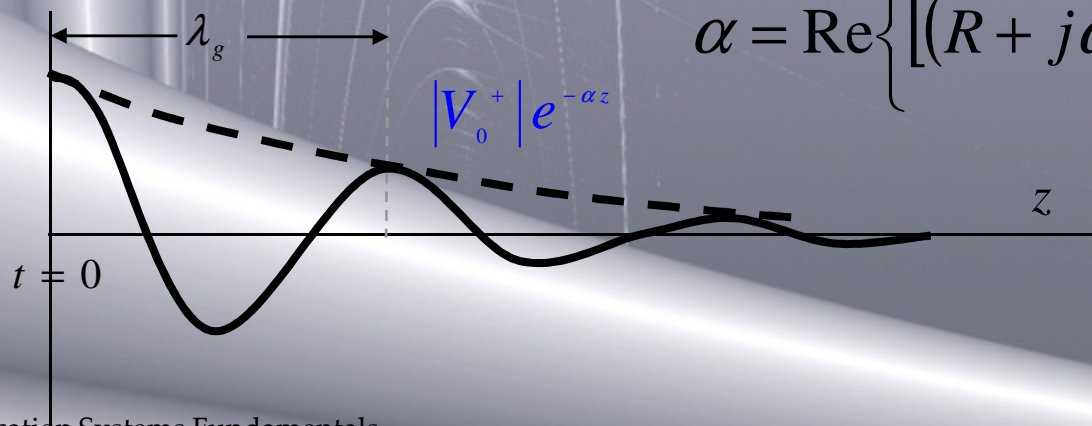
- Attenuation

$$V^+(z) = V_0^+ e^{-\gamma z} = V_0^+ e^{-\alpha z} e^{-j\beta z}$$

$$|V^+(z)| = |V_0^+ e^{-\gamma z}| = |V_0^+| |e^{-\alpha z}| |e^{-j\beta z}| = |V_0^+| |e^{-\alpha z}|$$

$$|e^{-\alpha z}| = \text{attenuation}$$

$$\alpha = \text{Re} \left\{ \left[(R + j\omega L)(G + j\omega C) \right]^{\frac{1}{2}} \right\}$$

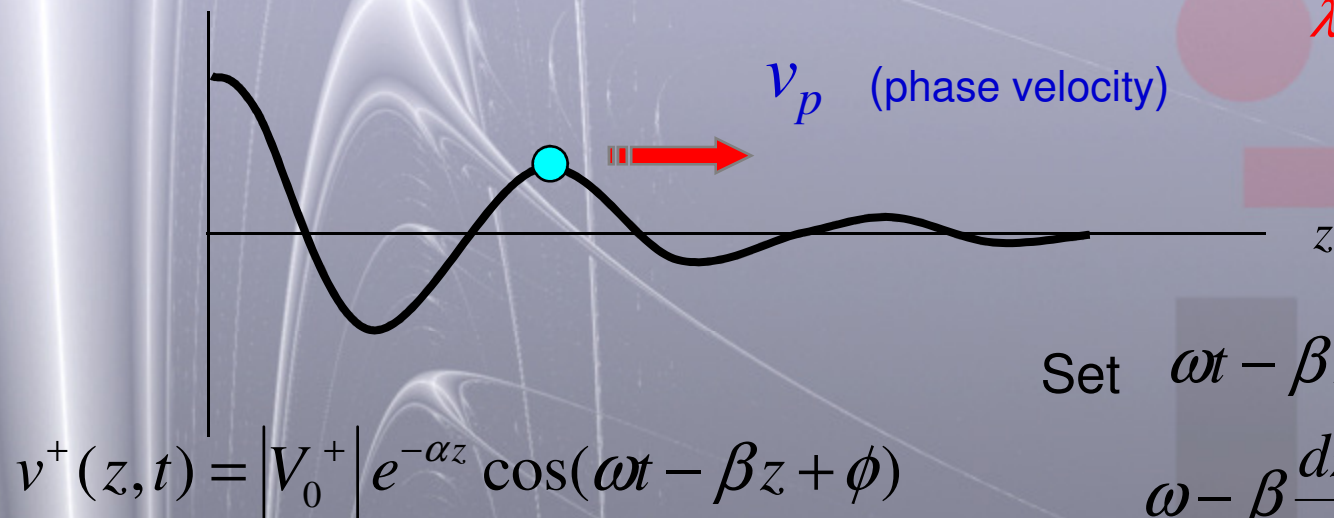


Transmission Line Secondary Parameters

- Phase Velocity

guided wavelength $\equiv \lambda_g$

$$\lambda_g = \frac{2\pi}{\beta} [\text{m}]$$



Set $\omega t - \beta z = \text{constant}$

$$\omega - \beta \frac{dz}{dt} = 0$$

$$\frac{dz}{dt} = \frac{\omega}{\beta}$$

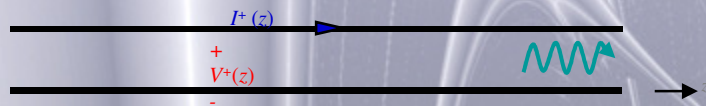
Hence
$$v_p = \frac{\omega}{\beta}$$

In expanded form:

$$v_p = \frac{\omega}{\text{Im}\{[(R + j\omega L)(G + j\omega C)]^{1/2}\}}$$

Transmission Line Secondary Parameters

- Characteristic Impedance Z_0



A wave is traveling in the positive z direction.

$$Z_0 \equiv \frac{V^+(z)}{I^+(z)}$$

$$V^+(z) = V_0^+ e^{-\gamma z}$$

$$I^+(z) = I_0^+ e^{-\gamma z}$$

$$Z_0 = \frac{V_0^+}{I_0^+}$$

(Z_0 is a number, not a function of position)

$$\frac{\partial v}{\partial z} = -Ri - L \frac{\partial i}{\partial t}$$

$$\begin{aligned} \frac{dV}{dz} &= -RI - j\omega LI \\ &= -ZI \end{aligned}$$

$$-\gamma V_0^+ e^{-\gamma z} = -ZI_0^+ e^{-\gamma z}$$

$$Z_0 = \frac{V_0^+}{I_0^+} = \frac{Z}{\gamma} = \left(\frac{Z}{Y} \right)^{1/2}$$

$$Z = R + j\omega L$$

$$Y = G + j\omega C$$

$$Z_0 = \left(\frac{R + j\omega L}{G + j\omega C} \right)^{1/2}$$

Power-wise

- Power is proportional to the voltage squared

$$P(d) \propto e^{-2\alpha d}$$

- So, attenuation dependence with distance is

$$At = K e^{2\alpha d}$$

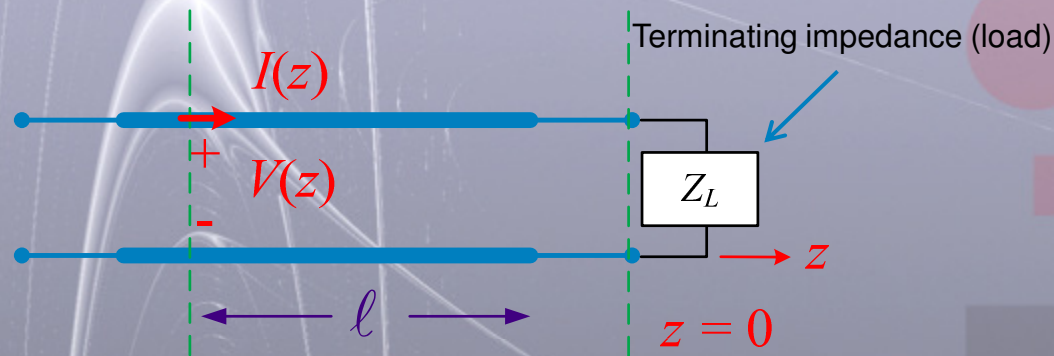
- When expressing it on dBs

$$At(dB) = K_1 + K_2 x$$

(constants vary with frequency)

Transmission Line Model

- When forward and backward traveling waves



$$V(z) = V_0^+ e^{-\gamma z} + V_0^- e^{+\gamma z} = V_0^+ e^{-\gamma z} \left(1 + \frac{V_0^-}{V_0^+} e^{2\gamma z} \right) = V_0^+ e^{-\gamma z} (1 + \Gamma_L e^{2\gamma z})$$

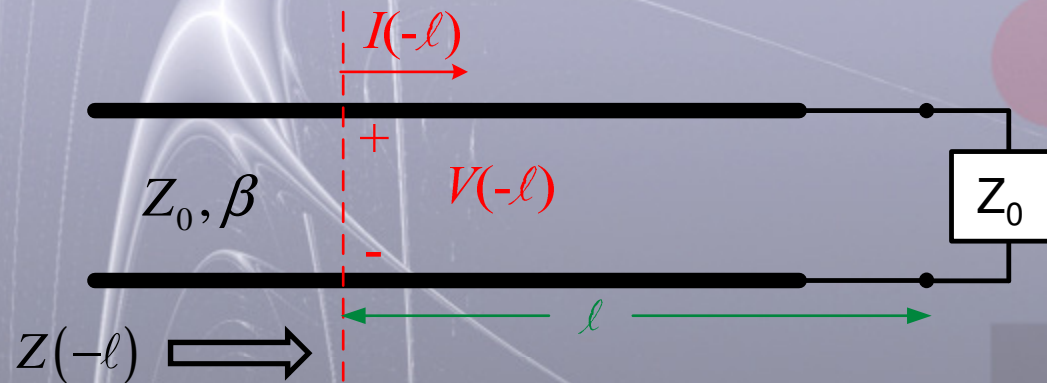
$$I(z) = \frac{1}{Z_0} [V_0^+ e^{-\gamma z} - V_0^- e^{+\gamma z}]$$

$\Gamma_L \equiv$ Load reflection coefficient

$$\Rightarrow \Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Impedance Matching in Transmission Lines

- Case 1: Matched load: ($Z_L = Z_0$)



$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = 0 \quad \leftarrow \text{No reflection from the load}$$

$$V(-\ell) = V_0 e^{+j\beta\ell}$$

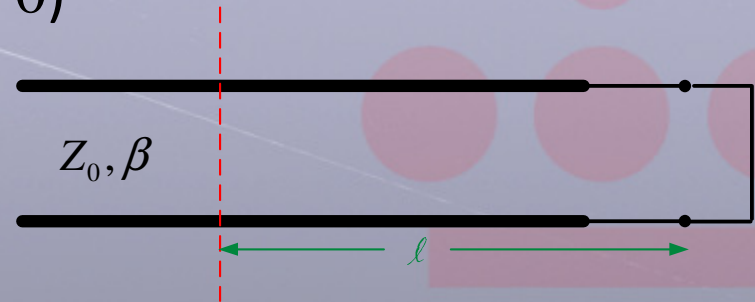
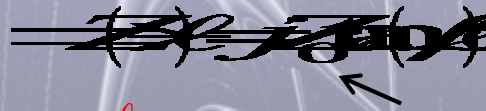
$$Z(-\ell) = Z_0 \quad \text{For any } \ell$$

$$I(-\ell) = \frac{V_0}{Z_0} e^{+j\beta\ell}$$

Impedance Matching in Transmission Lines

- Case 2: Short circuit load: ($Z_L = 0$)

$$\frac{Z_L}{Z_0} = 0$$

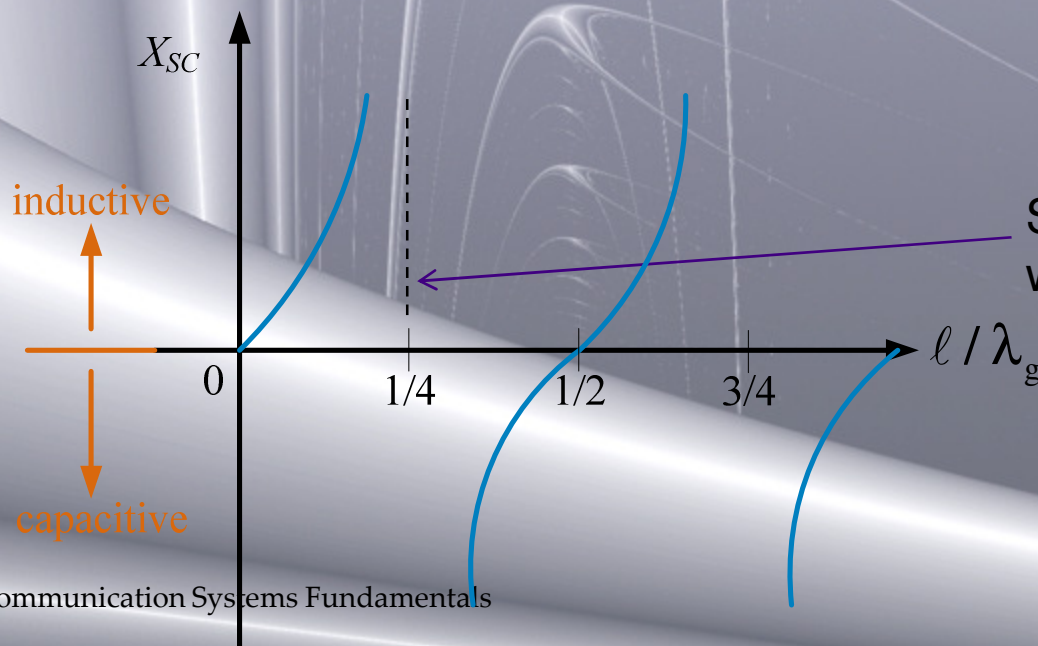


Note: $\beta l = 2\pi \frac{l}{\lambda_g}$

Always imaginary!

$$\Rightarrow Z_{in} = jX_c$$

$$X_c = Z_0 \tan(\beta l)$$



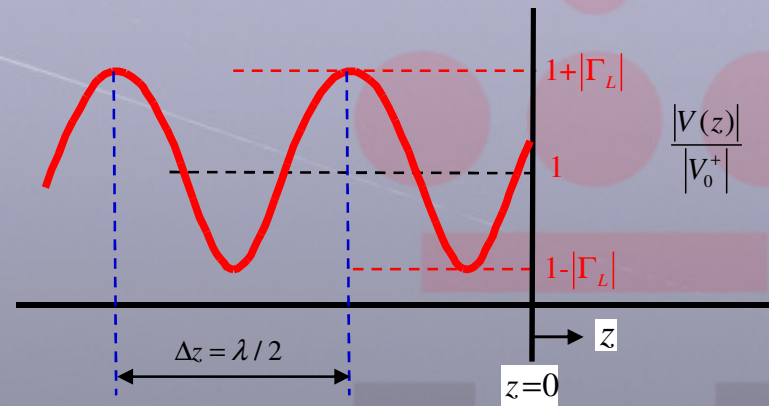
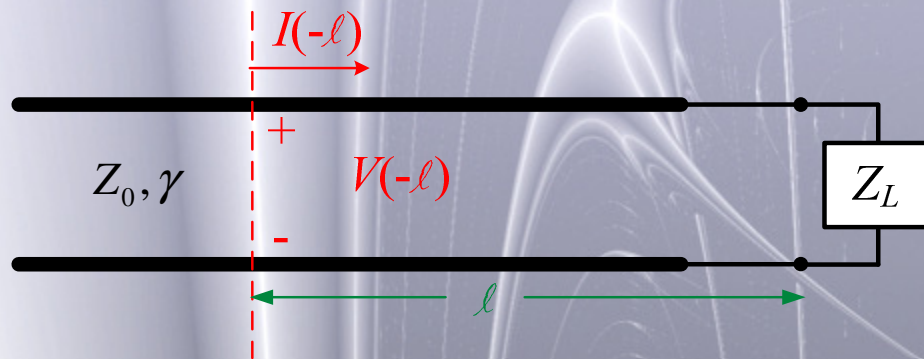
S.C. can become an O.C.
with a $\lambda_g/4$ trans. line

Impedance Matching in Transmission Lines

- Case 3: Open Circuit ($Z_L = \infty$)
 - Homework

Impedance Matching in Transmission Lines

- Voltage Standing Wave Ratio



$$V_{\max} = |V_0^+| (1 + |\Gamma_L|)$$

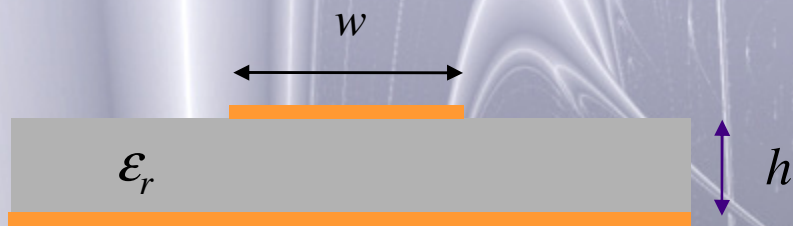
$$V_{\min} = |V_0^+| (1 - |\Gamma_L|)$$

$$\text{Voltage Standing Wave Ratio (VSWR)} = \frac{V_{\max}}{V_{\min}}$$

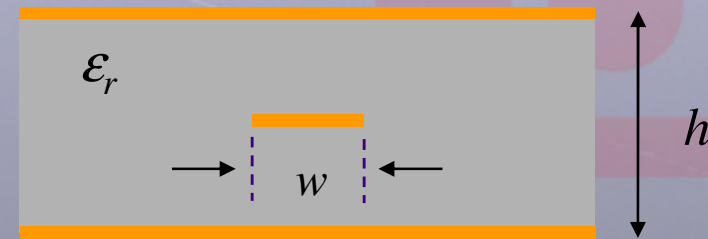
$$\text{VSWR} = \frac{1 + |\Gamma_L|}{1 - |\Gamma_L|}$$

Transmission Lines

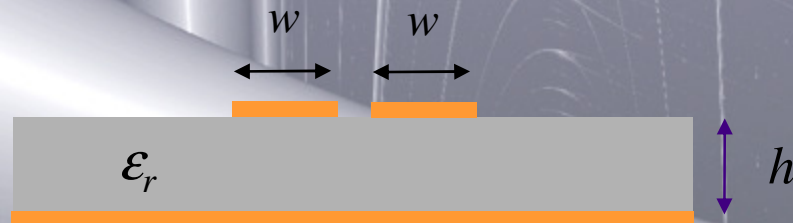
- Transmission lines commonly met on printed-circuit boards



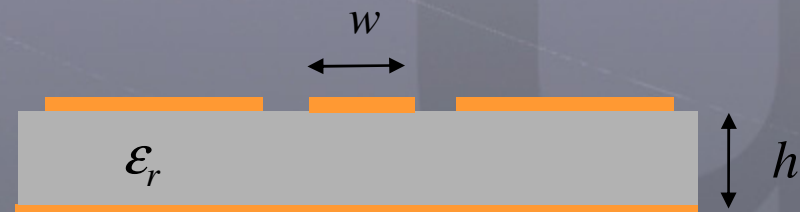
Microstrip



Stripline



Coplanar strips



Coplanar waveguide (CPW)

Transmission Lines

ϵ is electric permittivity

$\epsilon_0 = 8.85 \times 10^{-12} \text{ F/m}$ (free space)

ϵ_r is relative dielectric constant

Typical ϵ_r : 3.29 paper; 1 air;

3 to 4 polietilene and 4 to 6 PVC

μ is magnetic permeability

$\mu_0 = 4\pi \times 10^{-7} \text{ H/m}$ (free space)

μ_r is relative permeability

For most of dielectric materials, μ_r is close to one

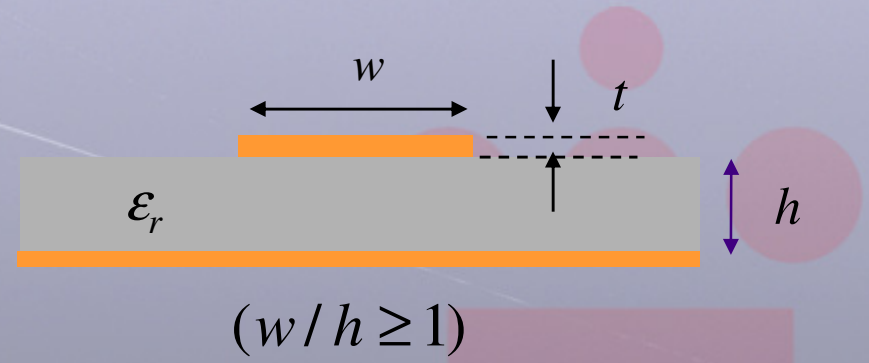
ρ is resistivity:

Cooper: 17.4; Bronze 19; Iron 120 ($\times 10^{-8} \Omega/\text{m}$)

$$\mu = \mu_r \mu_0;$$

$$\epsilon = \epsilon_r \epsilon_0$$

Microstrip Transmission Line



$$Z_0(f) = Z_0(0) \left(\frac{\epsilon_r^{eff}(f) - 1}{\epsilon_r^{eff}(0) - 1} \right) \sqrt{\frac{\epsilon_r^{eff}(0)}{\epsilon_r^{eff}(f)}}$$

$$Z_0(0) = \frac{120\pi}{\sqrt{\epsilon_r^{eff}(0)} \left[(w'/h) + 1.393 + 0.667 \ln \left((w'/h) + 1.444 \right) \right]}$$

$$w' = w + \frac{t}{\pi} \left(1 + \ln \left(\frac{2h}{t} \right) \right)$$

$$\epsilon_r^{eff}(f) = \left(\sqrt{\epsilon_r^{eff}(0)} + \frac{\sqrt{\epsilon_r} - \sqrt{\epsilon_r^{eff}(0)}}{1 + 4F^{-1.5}} \right)^2$$

$$\epsilon_r^{eff}(0) = \frac{\epsilon_r + 1}{2} + \left(\frac{\epsilon_r - 1}{2} \right) \left(\frac{1}{\sqrt{1 + 12(h/w)}} \right) - \left(\frac{\epsilon_r - 1}{4.6} \right) \left(\frac{t/h}{\sqrt{w/h}} \right)$$

Copper Pair / Twisted Pair

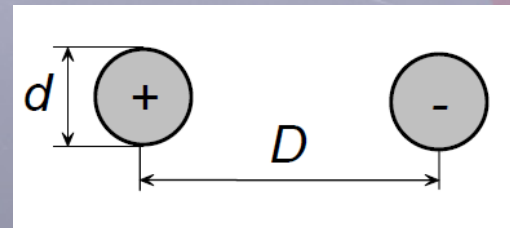
- Primary parameters of a Copper Pair

$$L = 2.3 \frac{\mu}{\pi} \log \left(2 \frac{D}{d} \right)$$

$$R = 2 \frac{\rho}{\pi d^2}$$

$$C = 0,43 \frac{\pi \epsilon}{\log \left(\frac{2D}{d} \right)}$$

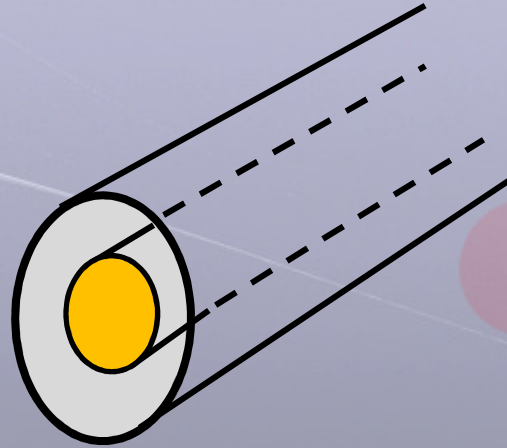
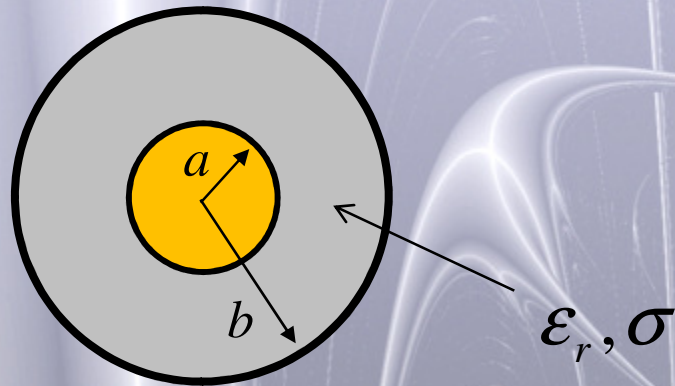
G: conductance depends on the dielectric, usually negligible but depending on the frequency



- D: Distance between cables
- d: diameter of each cable

$$Z_0 = 120 \cosh^{-1} \left(\frac{D}{d} \right) \\ \approx 276 \log \left(\frac{2D}{d} \right)$$

Coaxial Cable



$$C = \frac{2\pi\epsilon_0\epsilon_r}{\ln\left(\frac{b}{a}\right)} \quad [\text{F/m}]$$

$$R = \rho \left(\frac{1}{2\pi a} + \frac{1}{2\pi b} \right)$$

$$L = \frac{\mu_0\mu_r}{2\pi} \ln\left(\frac{b}{a}\right) \quad [\text{H/m}]$$

$$G = \frac{2\pi\sigma}{\ln\left(\frac{b}{a}\right)} \quad [\text{S/m}]$$

Summary of Concepts in this Chapter

- What are the primary parameters of the transmission lines
- Calculation of attenuation, and propagation velocity for transmission lines
- Calculate above parameters for common transmisión lines