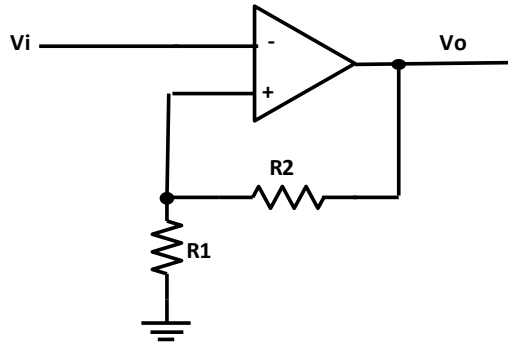


TEMA 6: EL TEMPORIZADOR INTEGRADO 555

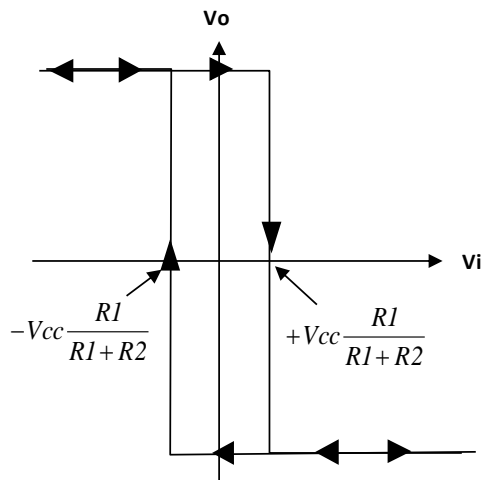
Introducción: Multivibrador monoestable

(Generación de pulsos de tensión con señal externa de disparo)

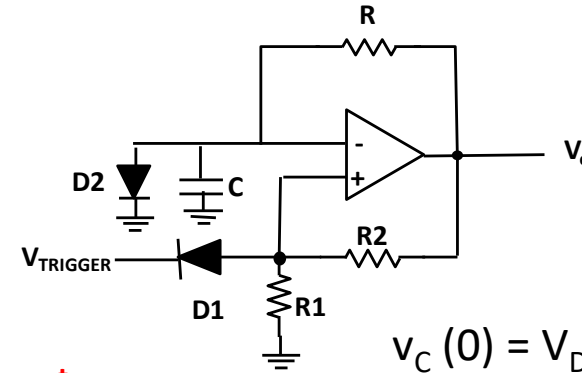
Disparador Schmitt



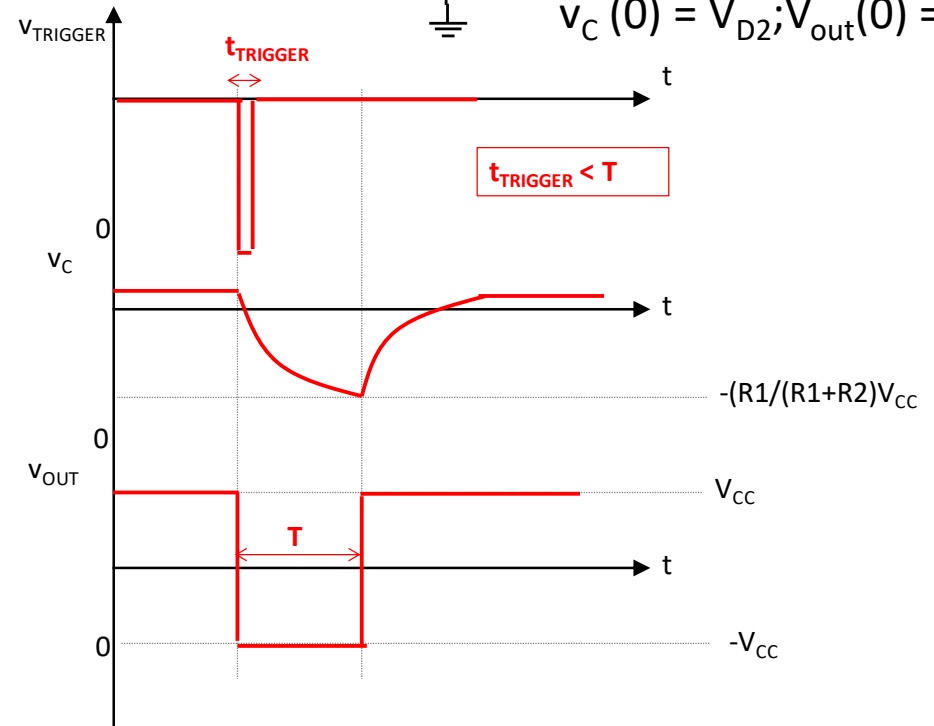
Función de transferencia



Multivibrador monoestable



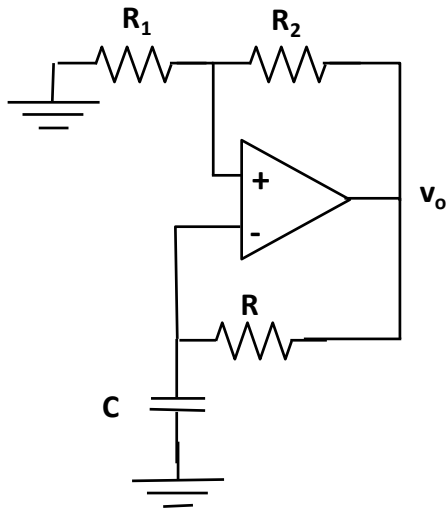
$$v_C(0) = V_{D2}; v_{out}(0) = +V_{CC}$$



Introducción: Multivibrador astable

(Autodisparado: generación continua pulsos de tensión)

Oscilador de relajación



Formas de onda

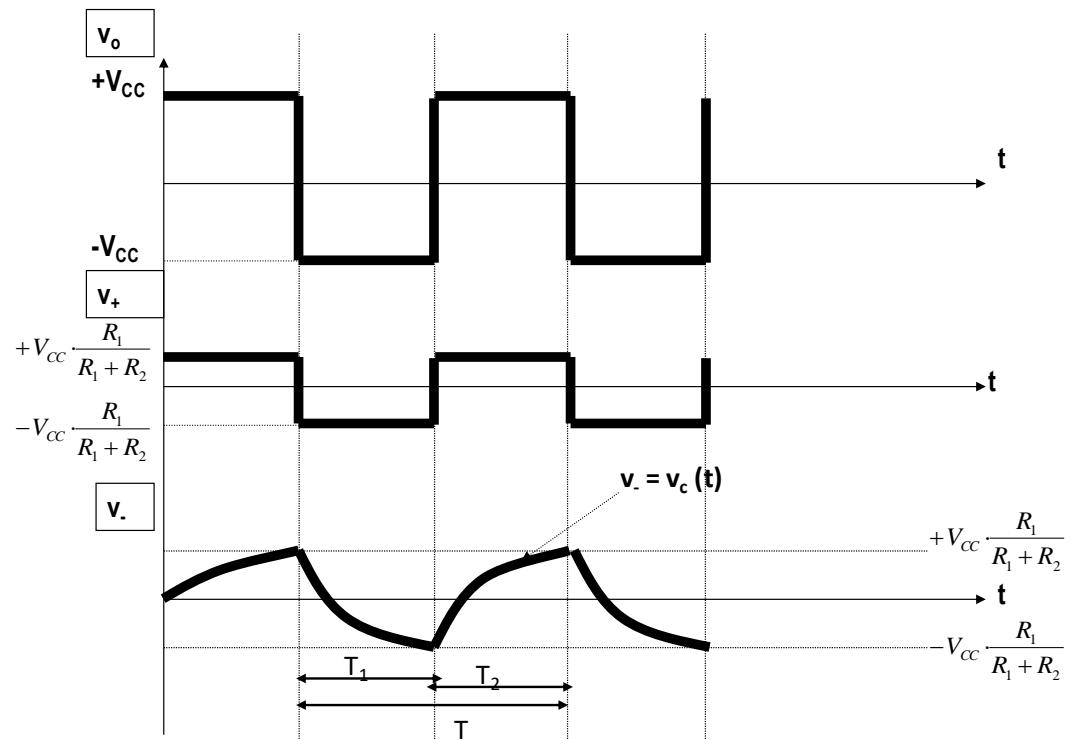
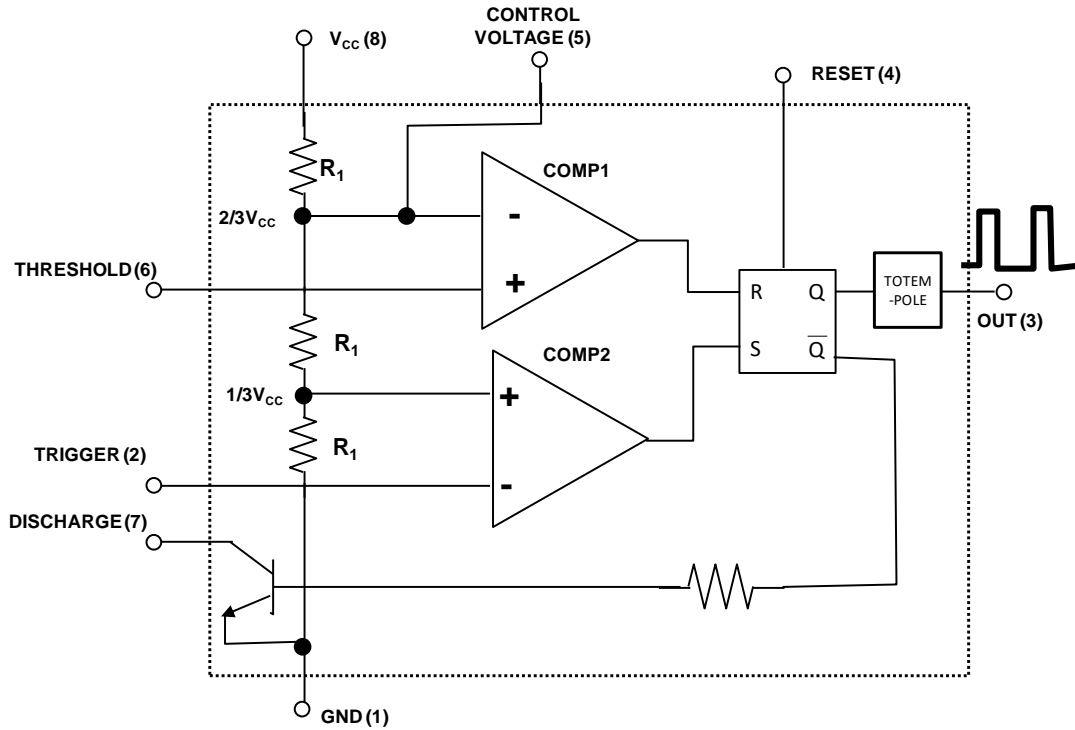
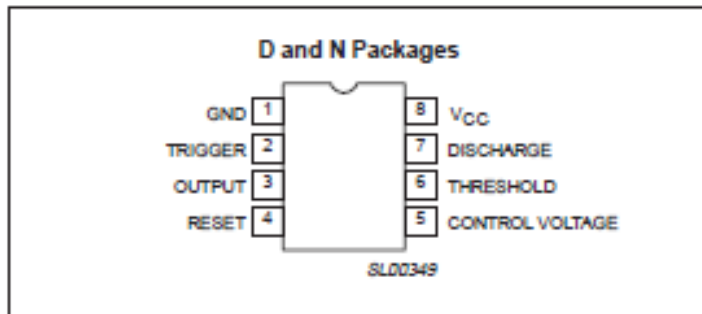


Diagrama de bloques



PIN CONFIGURATION



Modos de funcionamiento:

- Modo monoestable: Señal externa disparo (TRIGGER)
- Modo astable: Autodisparo (TRIGGER = THRESHOLD)

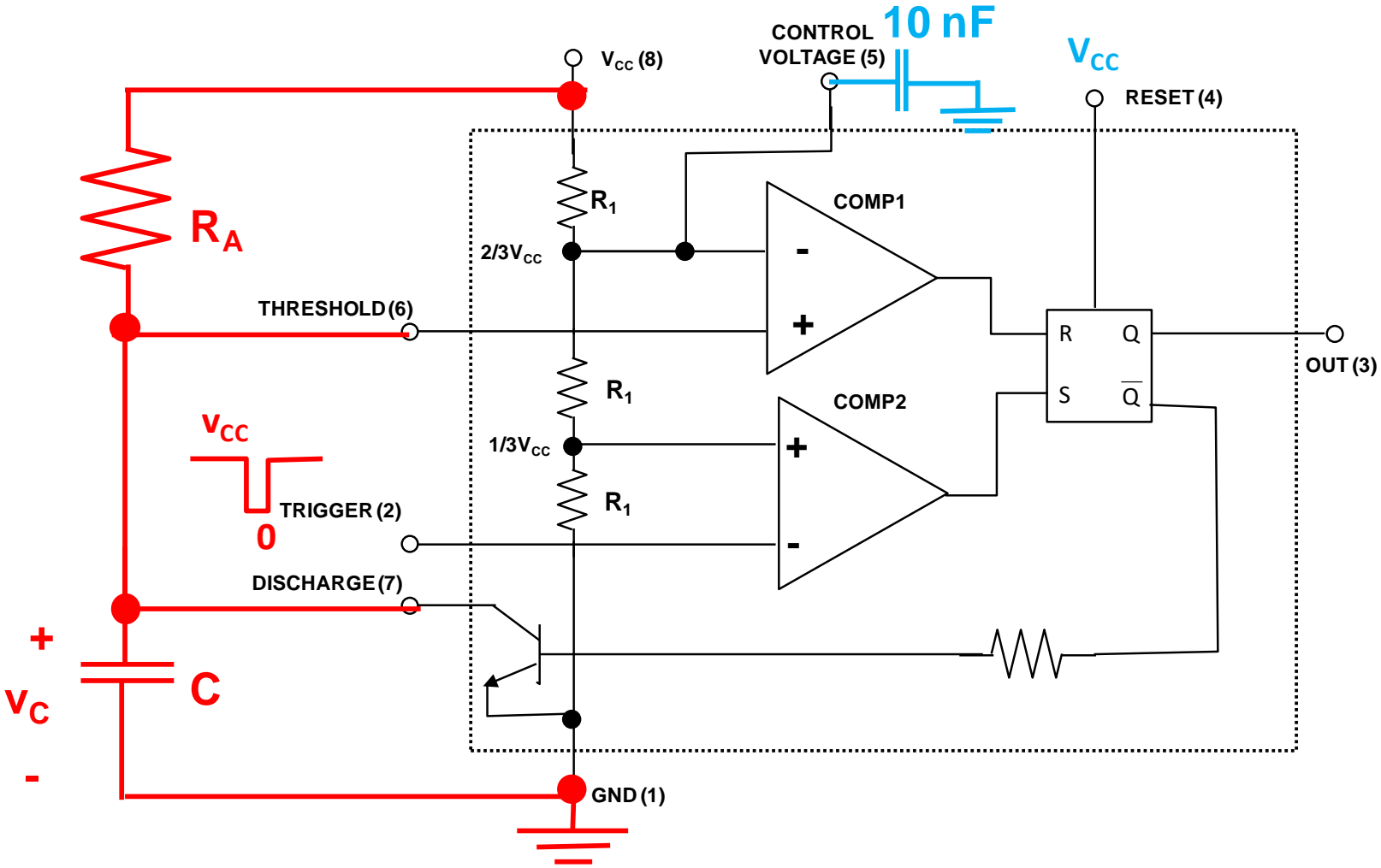
Bistable RS

R	S	Q_t
0	0	Q_{t-1}
0	1	1
1	0	0
1	1	X

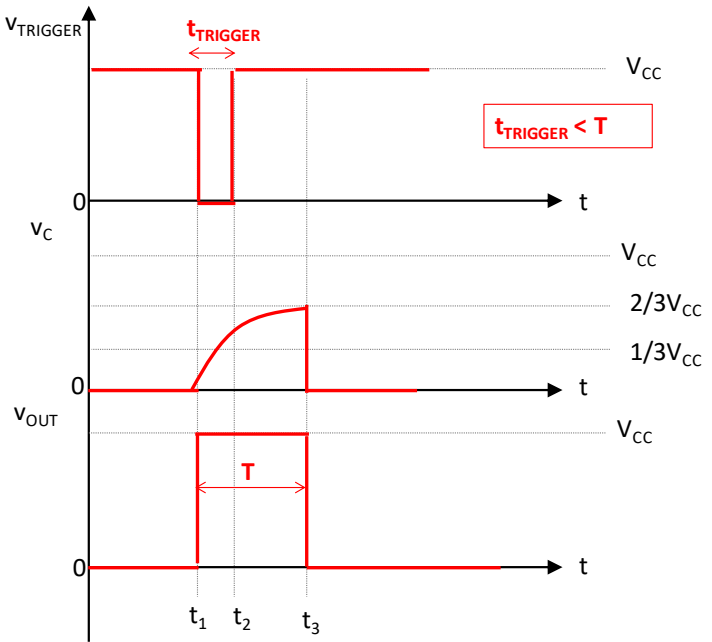
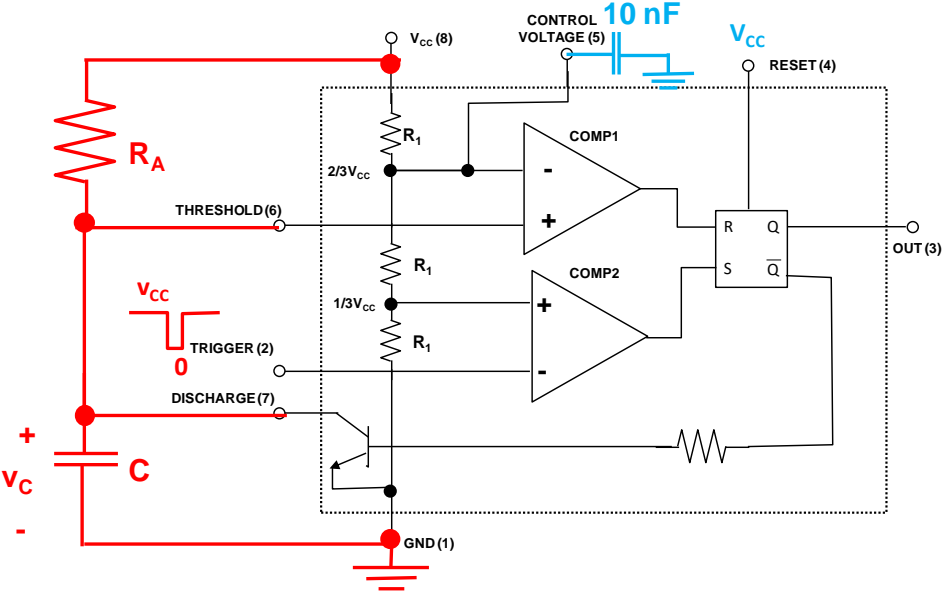
"1" $\rightarrow V_{CC}$

"0" $\rightarrow GND (0V)$

Modo monoestable

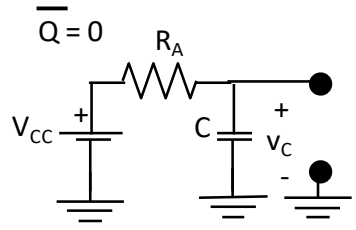
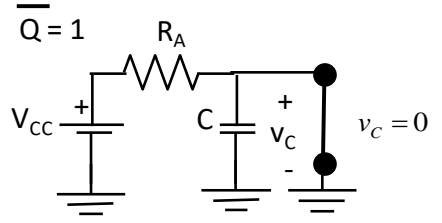


Modo monoestable



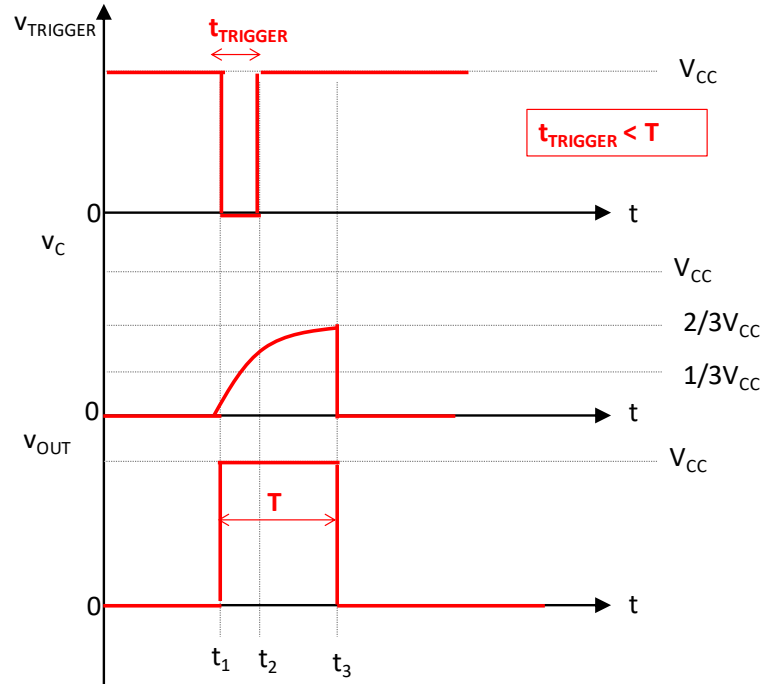
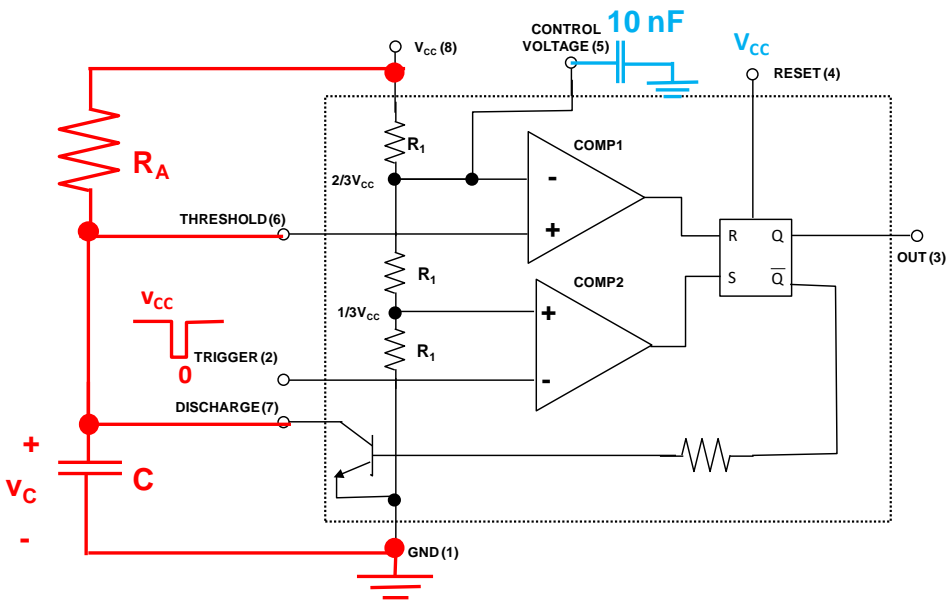
$v_C(0) = 0; V_{out}(0) = 0$

	COMP1			COMP2					
t	V ₊	V ₋	R	V ₊	V ₋	S	V _{OUT}	\overline{Q}	v _C
[0-t ₁)	0	2/3V _{cc}	0	1/3V _{cc}	V _{cc}	0	0	1	0
t ₁	0	2/3V _{cc}	0	1/3V _{cc}	0	1	1	0	v _C (t)
(t ₁ -t ₂)	v _C (t)	2/3V _{cc}	0	1/3V _{cc}	0	1	1	0	v _C (t)
[t ₂ -t ₃)	v _C (t)	2/3V _{cc}	0	1/3V _{cc}	V _{cc}	0	1	0	v _C (t)
t ₃	↑2/3V _{cc}	2/3V _{cc}	1	1/3V _{cc}	V _{cc}	0	0	1	0
>t ₃	0	2/3V _{cc}	0	1/3V _{cc}	V _{cc}	0	0	1	0

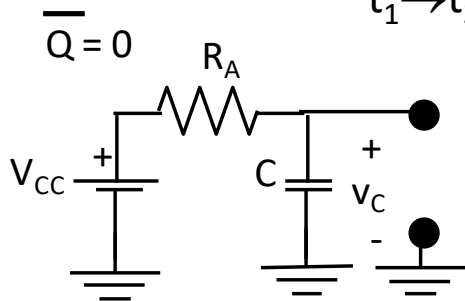


$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)})e^{-\frac{t}{\tau}} \quad 6$$

Modo monoestable



$t_1 \rightarrow t_3$: carga del condensador

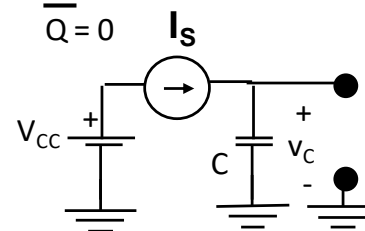
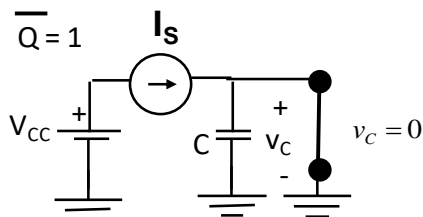
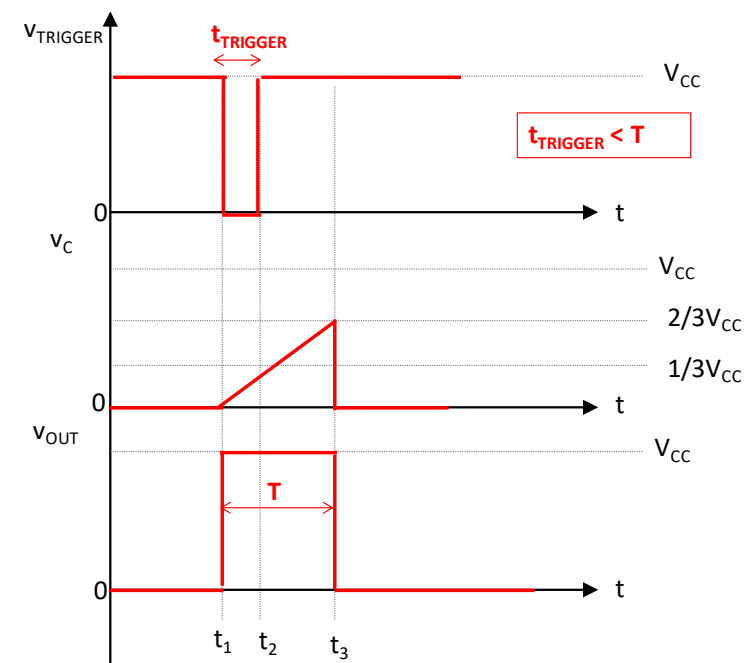
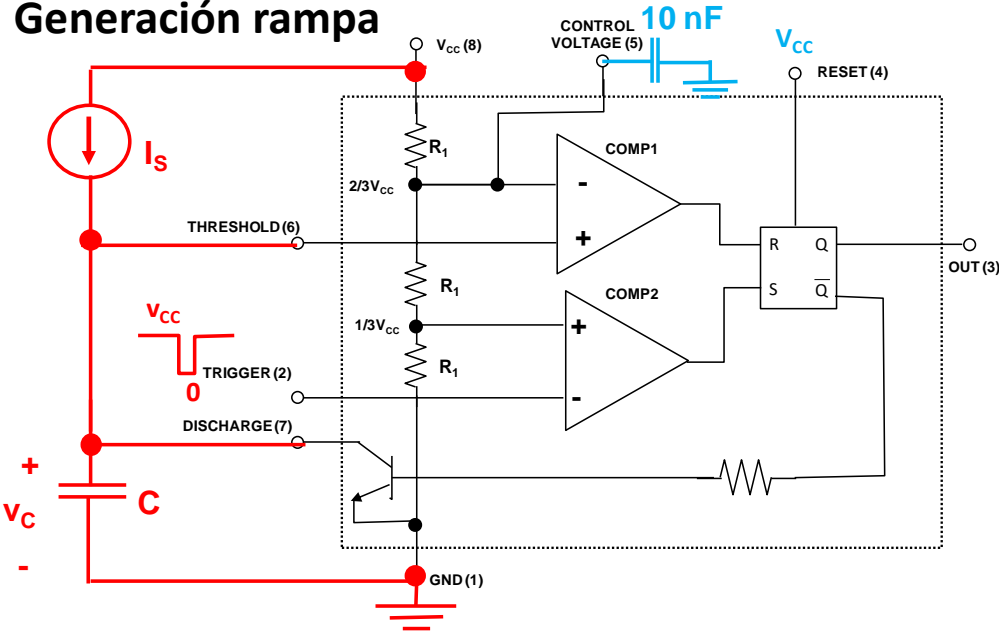


$$v_C(T) = V_{CC} + (0 - V_{CC}) \cdot e^{-\frac{T}{R_A \cdot C}} = \frac{2}{3} V_{CC}$$

$$\Rightarrow T = -R_A \cdot C \cdot \ln\left(\frac{1}{3}\right) \Rightarrow T = R_A \cdot C \cdot \ln(3) = 1.1 \cdot R_A \cdot C$$

$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) \cdot e^{-\frac{t}{\tau}}$$

Generación rampa

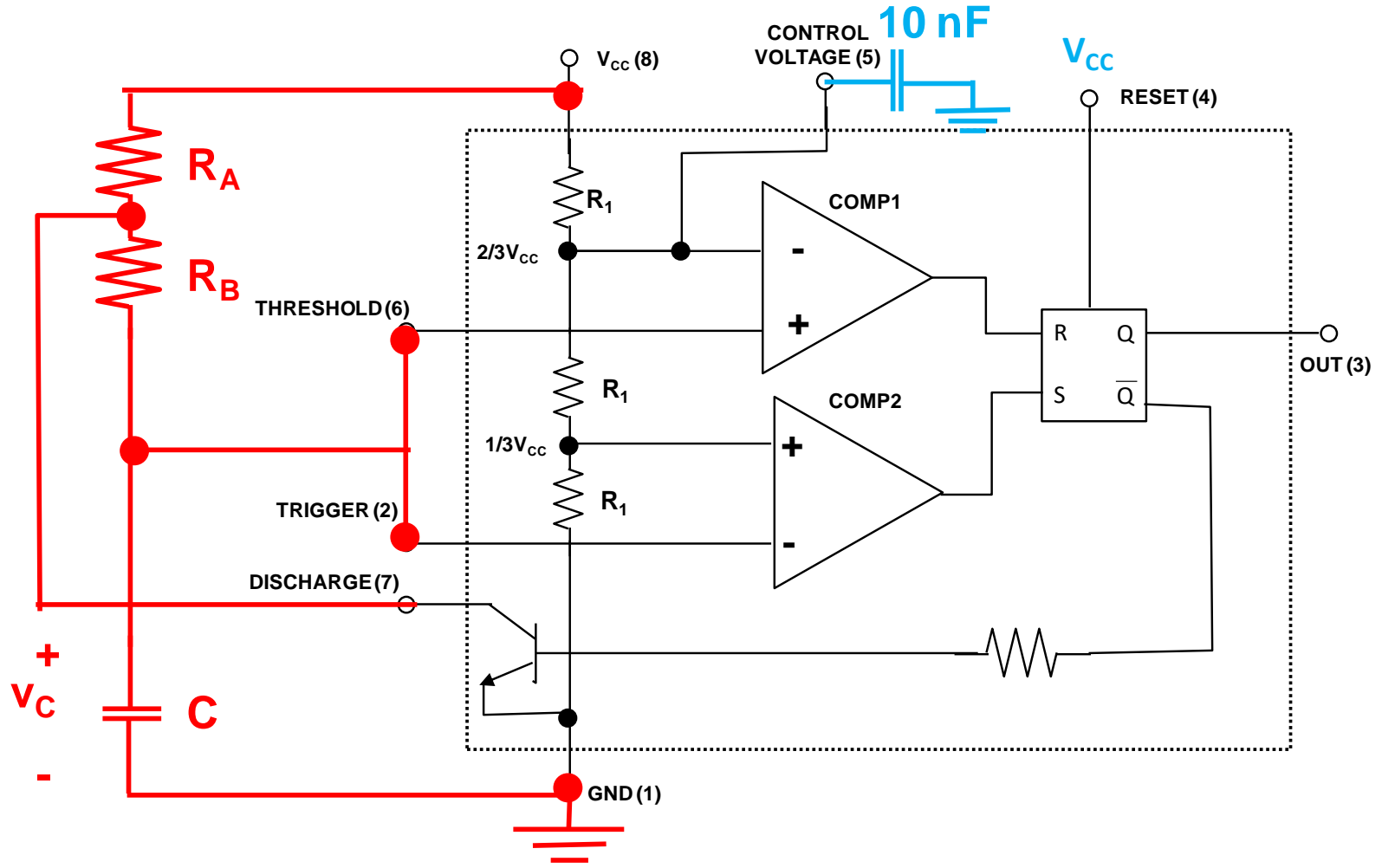


$$I_S = i_C = C \frac{dv_C}{dt} \Rightarrow v_C(t) = \frac{1}{C} \int I_S dt + v_C(0)$$

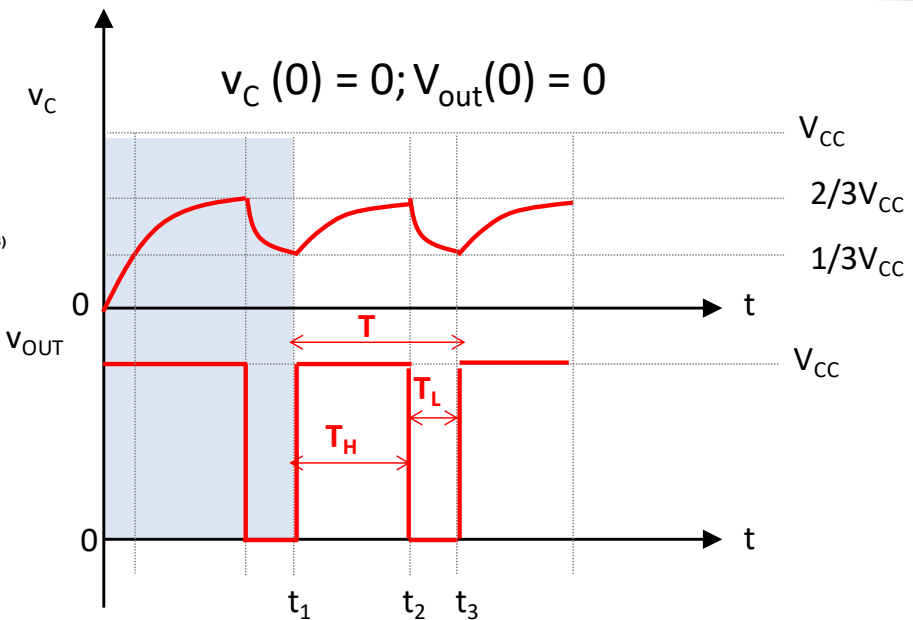
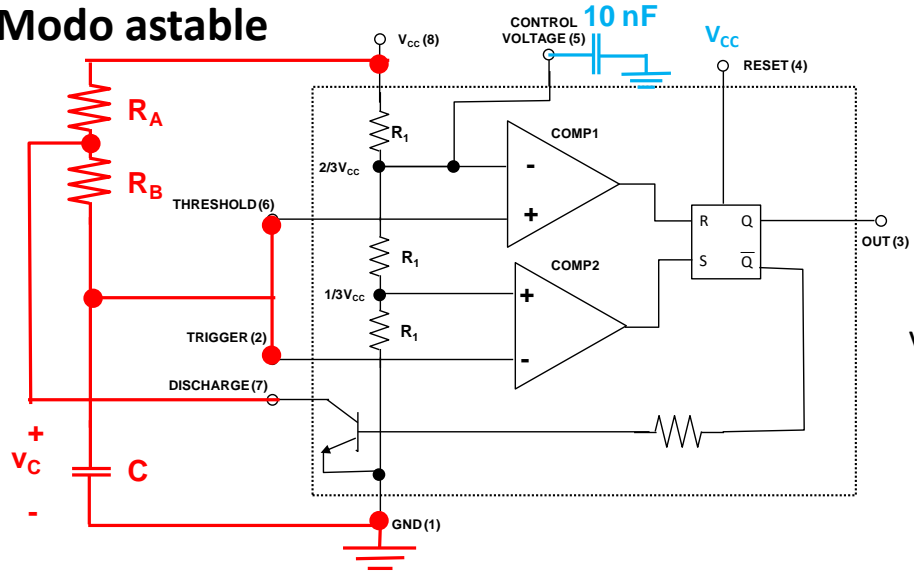
$t_1 \rightarrow t_3$: carga del condensador (corriente constante)

$$v_C(T) = \frac{1}{C} \cdot \int_0^T I_S dt + v_C(0) = \frac{2}{3} V_{CC} \Rightarrow \frac{T \cdot I_S}{C} = \frac{2}{3} V_{CC} \Rightarrow T = \frac{2}{3} V_{CC} \cdot \frac{C}{I_S}$$

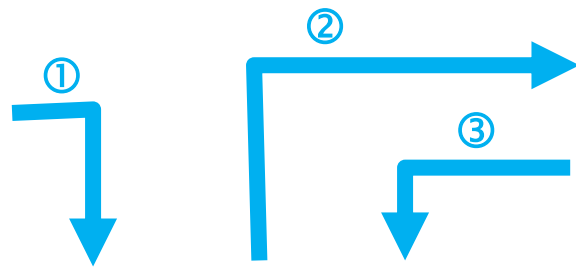
Modo astable



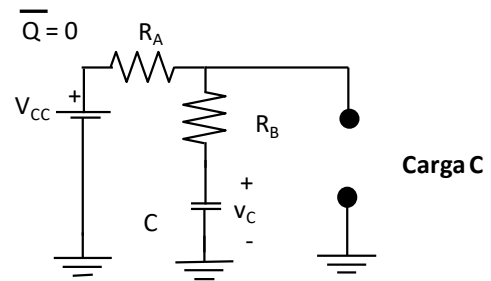
Modo astable



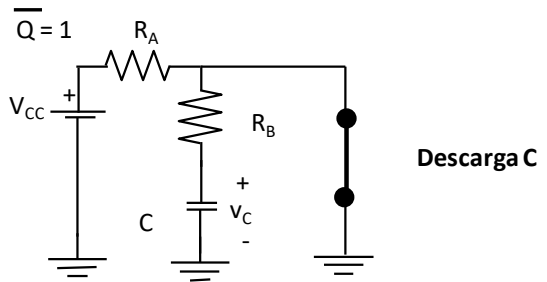
$t = t_1 : v_C(t) \downarrow \frac{1}{3} V_{CC}$
 $\Rightarrow \begin{cases} R = 0 \\ S = 1 \end{cases} \Rightarrow \begin{cases} V_{OUT} = 1 \\ \bar{Q} = 0 \end{cases} \Rightarrow \text{Carga } C$



$t = t_2 : v_C(t) \uparrow \frac{2}{3} V_{CC}$
 $\Rightarrow \begin{cases} R = 1 \\ S = 0 \end{cases} \Rightarrow \begin{cases} V_{OUT} = 0 \\ \bar{Q} = 1 \end{cases} \Rightarrow \text{Descarga } C$



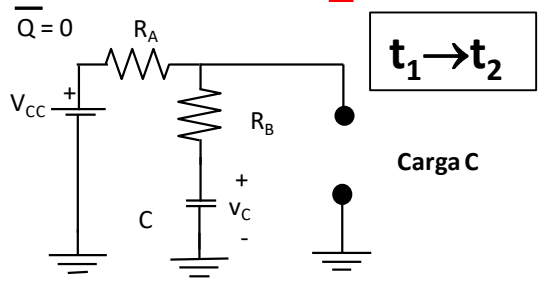
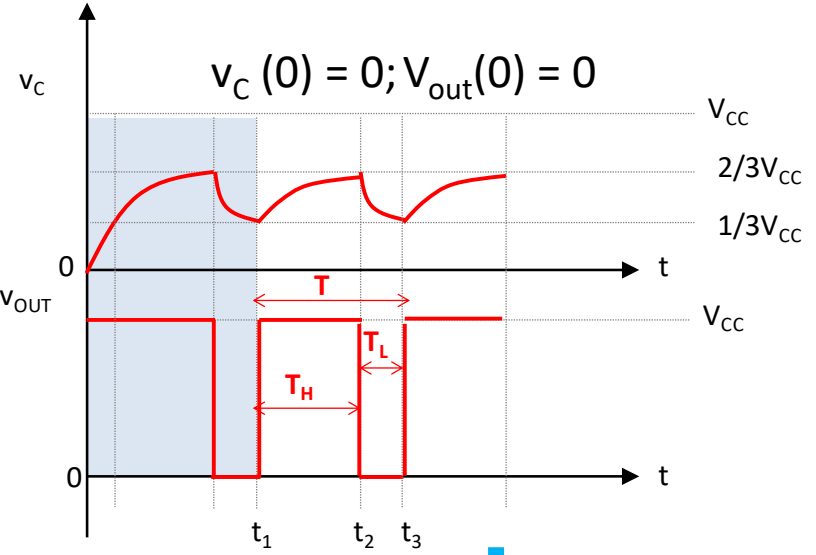
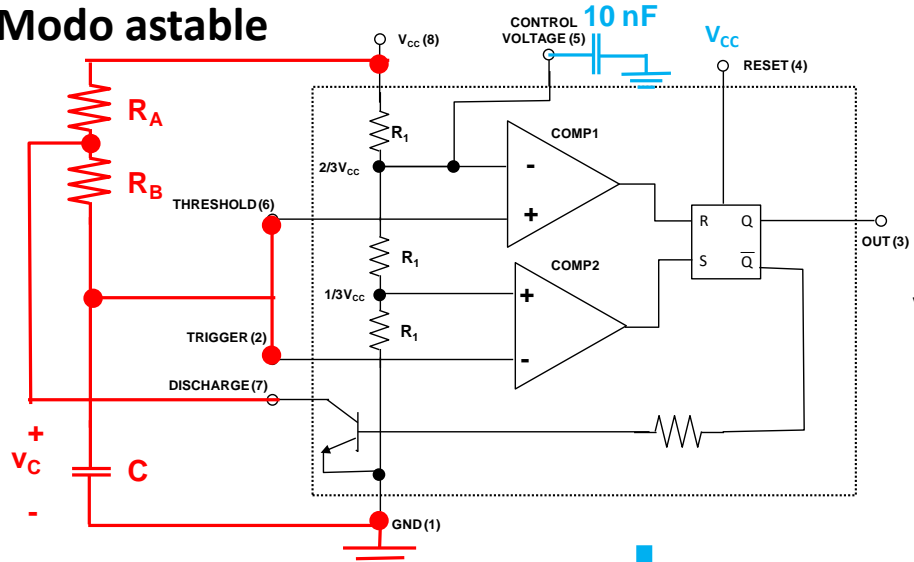
$t_2 > t > t_1$
 $t_3 > t > t_2$
 $\Rightarrow \frac{2}{3} V_{CC} > v_C(t) > \frac{1}{3} V_{CC}$
 $\Rightarrow \begin{cases} R = 0 \\ S = 0 \end{cases} \Rightarrow \begin{cases} V_{OUT} = V_{OUT-1} \\ \bar{Q} = \bar{Q}_{-1} \end{cases}$



$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) e^{-\frac{t}{(R_A + R_B) \cdot C}}$$

$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) e^{-\frac{t}{R_B \cdot C}} \quad 10$$

Modo astable

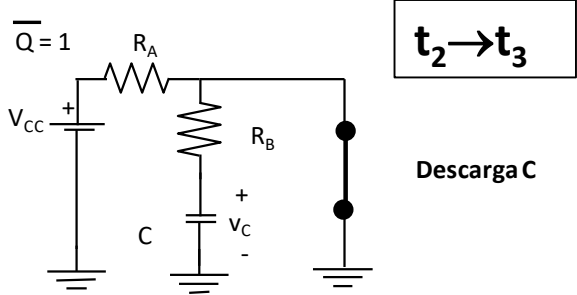


$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) e^{-\frac{t}{(R_A + R_B) \cdot C}}$$

$$v_C(T_H) = V_{CC} + \left(\frac{1}{3} V_{CC} - V_{CC} \right) \cdot e^{-\frac{T_H}{(R_A + R_B) \cdot C}} = \frac{2}{3} V_{CC}$$

$$\Rightarrow T_H = -(R_A + R_B) \cdot C \cdot \ln\left(\frac{1}{2}\right) \Rightarrow$$

$$T_H = (R_A + R_B) \cdot C \cdot \ln(2) = 0.7 \cdot (R_A + R_B) \cdot C$$



$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) e^{-\frac{t}{R_B \cdot C}}$$

$$v_C(T_L) = 0 + \left(\frac{2}{3} V_{CC} - 0 \right) \cdot e^{-\frac{T_L}{(R_B) \cdot C}} = \frac{1}{3} V_{CC}$$

$$\Rightarrow T_L = -(R_B) \cdot C \cdot \ln\left(\frac{1}{2}\right) \Rightarrow T_L = (R_B) \cdot C \cdot \ln(2) = 0.7 \cdot R_B \cdot C$$

$$T = T_H + T_L = \ln(2) \cdot C \cdot (R_A + 2R_B)$$

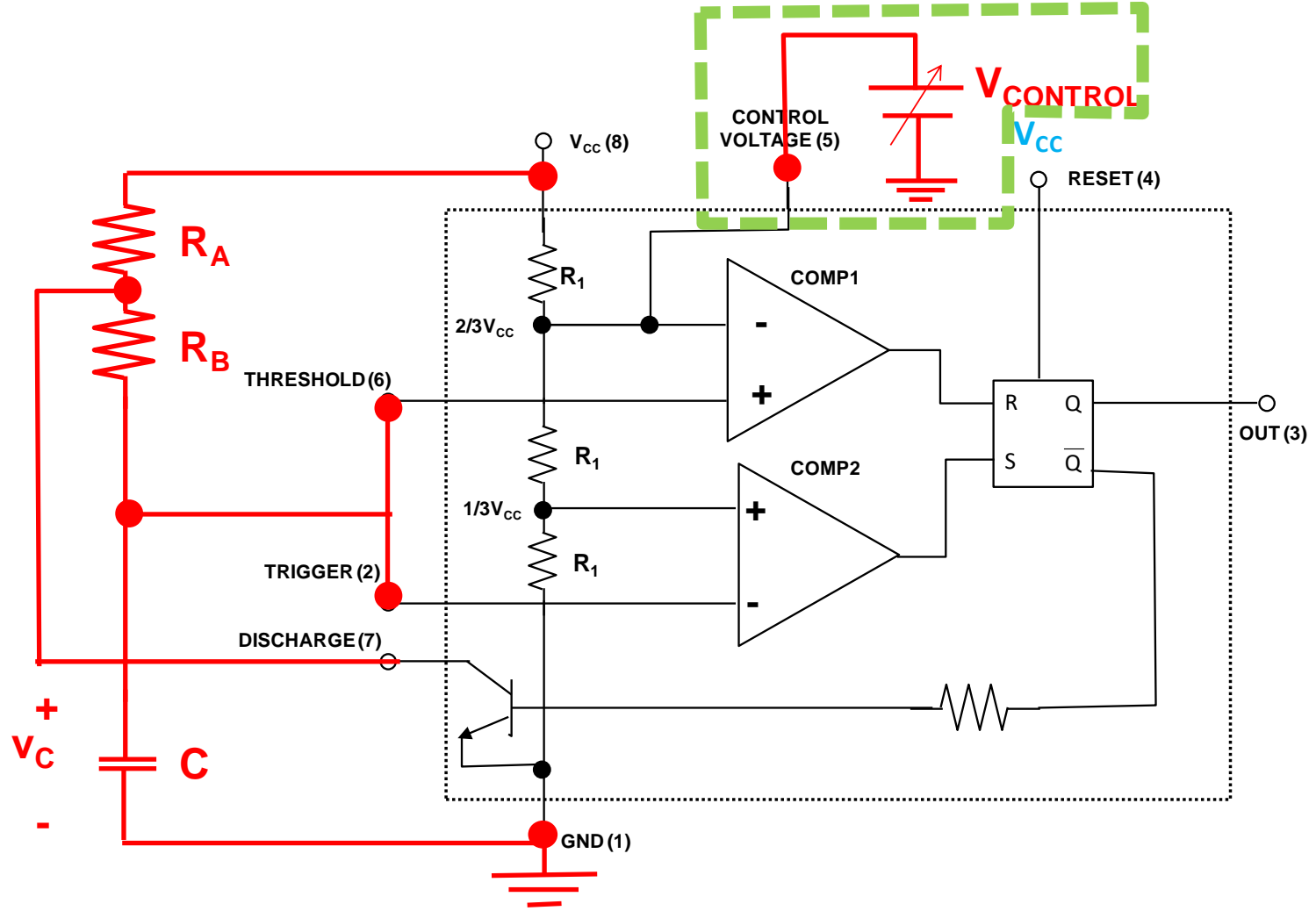
$$CT(\%) = \frac{T_H}{T} \cdot 100$$

$$CT(\%) = \frac{\ln(2) \cdot C \cdot (R_A + R_B)}{\ln(2) \cdot C \cdot (R_A + 2R_B)} \cdot 100$$

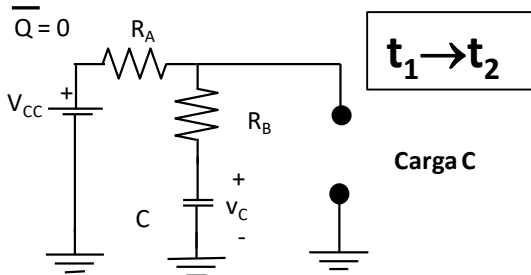
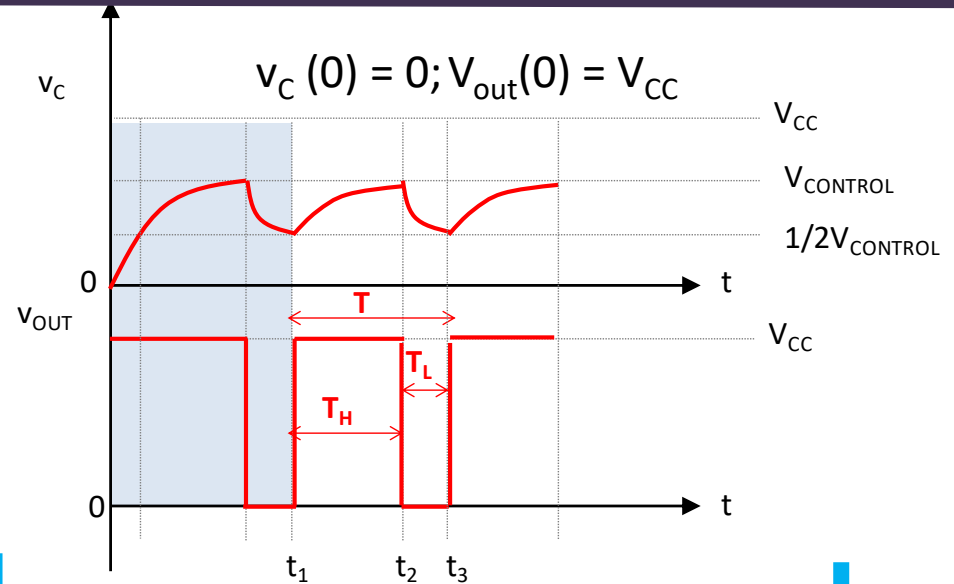
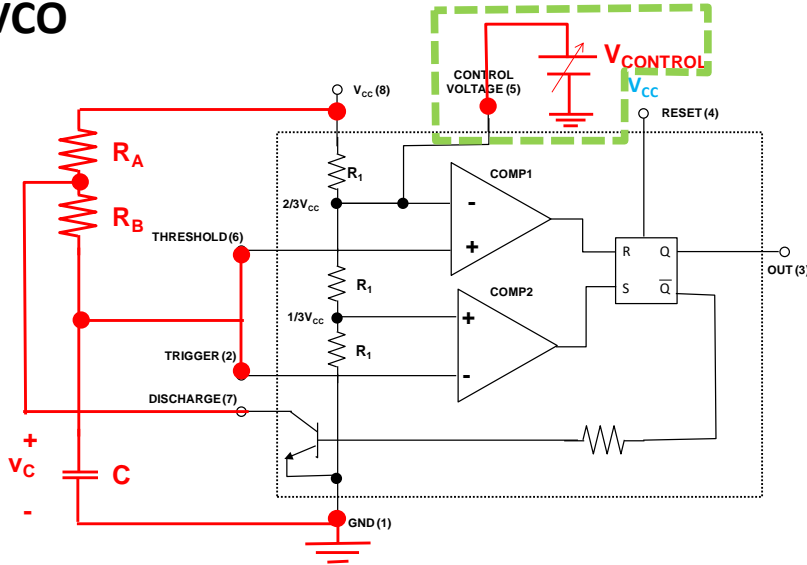
$$CT(\%) = \frac{R_A + R_B}{R_A + 2R_B} \cdot 100 > 50\%$$

$$CT(\%) \approx 50\% \Rightarrow R_A \ll R_B$$

VCO



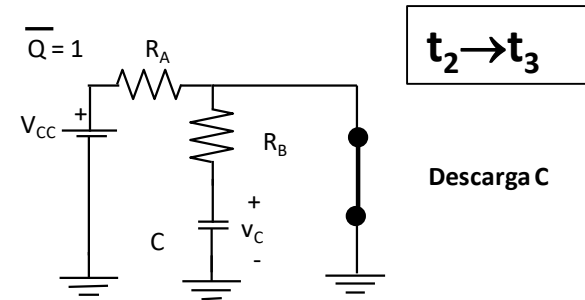
VCO



$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) e^{-\frac{t}{(R_A + R_B) \cdot C}}$$

$$v_C(T_H) = V_{CC} + \left(\frac{1}{2} V_{CONTROL} - V_{CC} \right) \cdot e^{-\frac{T_H}{(R_A + R_B) \cdot C}} = V_{CONTROL}$$

$$\Rightarrow T_H = (R_A + R_B) \cdot C \cdot \ln \left(\frac{V_{CONTROL} - 2V_{CC}}{2V_{CONTROL} - 2V_{CC}} \right)$$



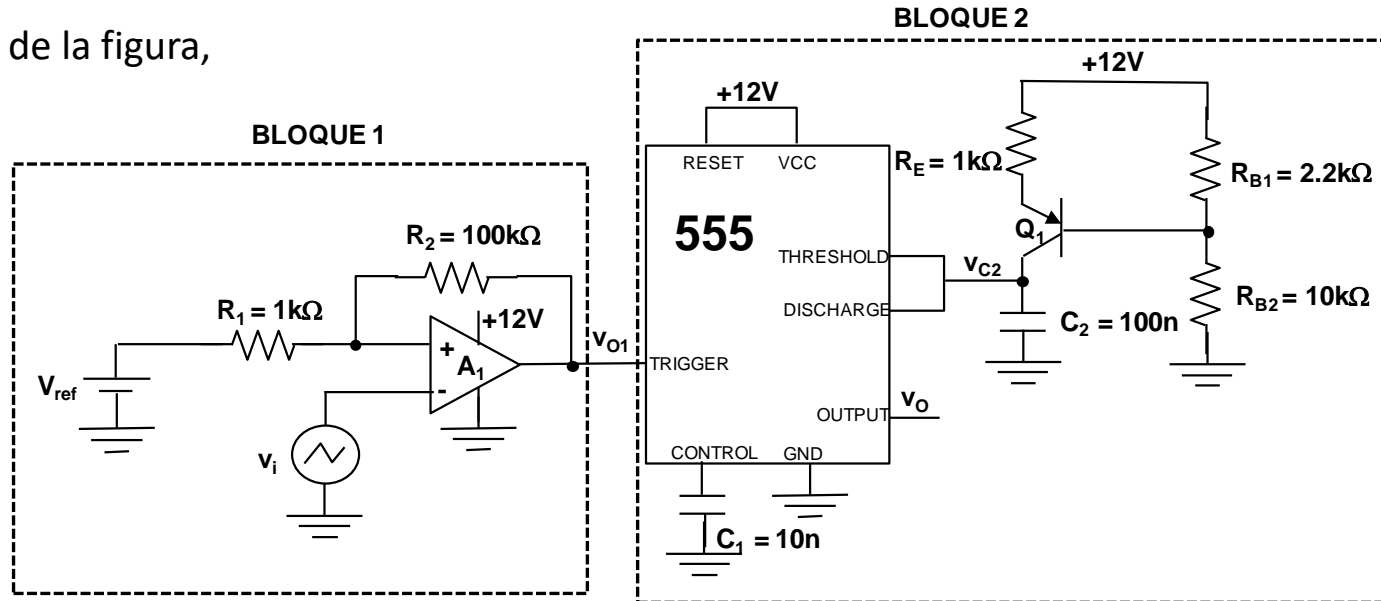
$$v_C(t) = v_{C(t \rightarrow \infty)} + (v_{C(t=0)} - v_{C(t \rightarrow \infty)}) e^{-\frac{t}{R_B \cdot C}}$$

$$v_C(T_L) = 0 + (V_{CONTROL} - 0) \cdot e^{-\frac{T_L}{R_B \cdot C}} = \frac{1}{2} V_{CONTROL}$$

$$\Rightarrow T_L = (R_B) \cdot C \cdot \ln(2) = 0.69 \cdot R_B \cdot C$$

EJERCICIO PROPUESTO

Dado el circuito de la figura,



Datos: A_1 : Amplificador operacional ideal

v_i : Señal triangular de 1kHz, 2.5V de amplitud y 2.5V de offset

Q_1 : $V_{BE\text{activa}} = 0.6V$, $V_{CE\text{sat}} = 0.2V$, $\beta = 250$

Se pide:

- Obtenga y represente la función de transferencia del primer bloque (v_{O1} en función de v_i).
- Deduzca el valor de la fuente de tensión continua, V_{ref} , para que el ciclo de trabajo de la tensión v_{O1} sea del 80%
- Describa el funcionamiento del segundo bloque y represente las señales v_{O1} , v_{C2} y v_O en función del tiempo, acotando los valores significativos en los ejes de tensión y tiempo e incluyendo todos los cálculos para la determinación de dichos valores.